

# APPLICATION UNDER UNITED STATES PATENT LAWS

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Invention: SENSOR FOR DETECTING QUANTITY OF LIGHT

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## This is a:

- ☐ Provisional Application
- ☒ Regular Utility Application
- ☐ Continuing Application
- ☐ PCT National Phase Application
- ☐ Design Application
- ☐ Reissue Application
- ☐ Plant Application
- ☐ Substitute Specification  
Sub. Spec. filed \_\_\_\_\_  
in App. No. \_\_\_\_\_ / \_\_\_\_\_
- ☐ Marked Up Specification re  
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## SPECIFICATION

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a  
SENSOR FOR DETECTING QUANTITY OF LIGHT  
INCIDENT ON A VEHICLE

CROSS REFERENCE TO RELATED APPLICATIONS

This application is based upon and claims the benefit  
5 of Japanese Patent Applications No. 10-329668 filed on  
November 19, 1998, and No. 11-60283 filed on March 8, 1999,  
the contents of which are incorporated herein by reference.

BACKGROUND OF THE INVENTION

10 1. Field of the Invention

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This invention relates to a sensor for detecting a  
quantity of light, which is applied to an automotive air  
conditioner, particularly to an air conditioning system  
capable of independently air-conditioning left and right  
15 sides of a vehicle.

2. Description of the Related Art

A so-called zone air-conditioning method (left-light  
side independently air-conditioning method) is a method  
for controlling an automotive air conditioner using a  
20 sensor, which detects a quantity (intensity) and a  
direction of solar radiation, to independently air-  
condition left and right sides in a vehicle compartment.

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25 As the sensor capable of detecting the quantity and  
direction of solar radiation, a 2D (two elements) type  
sensor has been developed. Referring to FIG. 22, the 2D  
type sensor has a left side detecting element  
(photodetector) 51 disposed at a right side of an axis  $L_{cont}$ ,  
which is a reference of  $0^\circ$  in azimuth, and a right side  
detecting element (photodetector) 52 disposed at a light

side of the axis  $L_{cent}$ . A shading member 54 having a through hole 53 is disposed above the detecting elements 51, 52. The right side detecting element 51 and the left side detecting element 52 receive light from the right side and the left side of the axis  $L_{cent}$ , respectively, and output signals corresponding to quantities of light. When azimuth  $\phi$  is  $0^\circ$ ,  $30^\circ$ ,  $60^\circ$ , or  $90^\circ$  as shown in FIGS. 4A to 4D, output ratios are as shown in FIG. 23. When azimuth  $\phi$  is  $0^\circ$ , right side and left side output ratios  $CR_R$ ,  $CR_L$  are 0.50, respectively. The left side and right side output ratios  $CR_L$ ,  $CR_R$  are represented by the following formulas:

$$CR_L = (\text{left side detecting element output current} \times R) / (\text{the sum of left side and right side detecting element output currents} \times R)$$

$$CR_R = (\text{right side detecting element output current} \times R) / (\text{the sum of left side and right side detecting element output currents} \times R)$$

In FIG. 23, shift between the shading member and the photodetectors is zero. Here, a relationship in position between the shading member 54 and the photodetectors 51, 52 is important to exhibit desirable characteristics, and is required to have an assembling accuracy of several tens  $\mu m$ . When positional shift of, for example, 0.1 mm occurs among the members, output ratios are as shown in FIG. 25. In this case, light irradiated parts when azimuth  $\phi$  is  $0^\circ$ ,  $30^\circ$ ,  $60^\circ$  and  $90^\circ$  are as shown in FIGS. 26A to 26D. When azimuth  $\phi$  is  $0^\circ$ , right side and left side output ratios  $CR_R$ ,  $CR_L$  are 0.60, 0.40, respectively. Thus, when the

positional shift occurs between the shading member 54, and the photodetectors 51, 52, there arises a large difference between the left side and right side output ratios, thereby causing malfunctions when left side and right sides in the compartment are independently air-conditioned. Further, requiring high accuracy for processing the parts inevitably results in high cost.

JP-A-7-43145 proposes a technique for forming a shading film by printing black epoxy resin on a transparent substrate disposed above a photodetector. A light transmittance hole is formed at the central portion of the shading film. Accordingly, the shading member is positioned with respect to the photodetector with high accuracy. However, this technique requires to visually recognize the photodetector when the resin is printed, resulting in low workability and low processing yield.

#### SUMMARY OF THE INVENTION

The present invention has been made in view of the above problems. An object of the present invention is to lessen an adverse effect caused by a positional shift between a shading member and a photodetector with desirable detection characteristics.

Here, detection characteristics required for a sensor will be explained. Elevation and azimuth are determined as shown in FIG. 27. FIG. 28 specifically indicates a relationship between the azimuth and a quantity of heat received by a vehicle when the sun moves from the front to the right side of the vehicle with the elevation

of 40°. The quantity of heat received by the vehicle becomes the maximum when the azimuth is 60°, and decreases in the order of 90°, 30°, and 0° azimuths. When the azimuth is in a range of 0° to 30°, the change in quantity of heat received by the vehicle is small, and sunlight is delivered uniformly to passengers. With this azimuth range, it is assumed that a difference in quantity of solar radiation between the left side and the right side is small. On the other hand, when the azimuth is larger than approximately 30°, the difference in quantity of solar radiation aimed to the passengers is large.

Accordingly, as shown in FIG. 29, it is desirable for the sensor that sensor outputs from the right and left sides are approximately equal to each other when the azimuth is in a range of 0° to 30°, and abruptly change (increase or decrease) when the azimuth is in a range of 30° to 60°. That is, the difference between the outputs from the right and left sides is not required when light enters from a vehicle front with the azimuth in a range of 0° to 30°. The difference between the outputs from the right and left sides is required to be large when the azimuth is larger than approximately  $\pm 30^\circ$ .

To achieve the above object with the desirable characteristics, according to the present invention, a sensor for detecting a quantity of light has a housing having an axis along a direction in which light enters the sensor when an azimuth is zero. The axis divides a surface of the housing into a first region and a second region. A first photodetector is disposed on the second region of

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the housing, and a second photodetector is disposed on the first region of the housing. A central photodetector is further disposed on both the first region and the second region across the axis. A sensitivity of the central photodetector is lowered as compared to those of the first and second photodetectors. A first quantity of light entering the sensor from a side of the first region is cooperatively detected by the first photodetector and the central photodetector, and a second quantity of light entering the sensor from a side of the second region is cooperatively detected by the second photodetector and the central photodetector.

Accordingly, when the sensor is mounted on a vehicle to detect quantities of light incident on right and left seats of the vehicle, the right and left seats can be independently air-conditioned based on the quantities of light detected by the sensor. In addition, because the sensitivity in the vicinity of the axis is blunted (lowered) by the central photodetector having a low sensitivity, even if a positional shift occurs between a shading member disposed above the housing and the photodetectors, output signals corresponding to the first and second quantities of light are less susceptible to the positional shift.

In other words, when the azimuth is small, light is incident on the vicinity of the axis. In this case, a difference between the output signals corresponding to the first and second quantities of light is small. When the azimuth increases, the difference between the output

signals also increases, thereby approaching ideal detection characteristics.

When the detection of the quantities of light is performed without using the central photodetector, the first photodetector has a plurality of first protrusions protruding from the second region toward the first region across the axis, and the second photodetector has a plurality of second protrusions protruding from the first region toward the second region across the axis. The plurality of first protrusions extend on the first region with a first width from the axis together with the plurality of second protrusions, and the plurality of second protrusions extend on the second region with a second width from the axis together with the plurality of first protrusions. Accordingly, the sensitivity of the vicinity of the axis is blunted, thereby achieving the effects described above.

#### BRIEF DESCRIPTION OF THE DRAWINGS

Other objects and features of the present invention will become more readily apparent from a better understanding of the preferred embodiments described below with reference to the following drawings, in which:

FIG. 1 is a plan view showing a sensor for detecting a quantity of light in a first preferred embodiment;

FIG. 2 is a cross-sectional view taken along line II-II in FIG. 1;

FIG. 3 is a plan view showing a sensor chip;

FIG. 4 is an explanatory view of the sensor chip;

FIG. 5 is a plan view showing a slit plate;

FIG. 6 is a cross-sectional view showing an optical path in the sensor;

FIG. 7 is a cross-sectional view showing an optical path in the sensor;

FIG. 8 is a cross-sectional view showing an optical path in the sensor;

FIG. 9 is a diagram showing an electrical constitution of an automatic air conditioning system;

FIG. 10 is a diagram showing a constitution of a signal processing circuit;

FIG. 11 is a graph showing a relationship between the azimuth and output ratios of the sensor with no positional shift;

FIGS. 12A to 12D are schematic views showing light irradiated parts when the azimuth is changed;

FIG. 13 is a graph showing a relationship between the azimuth and output ratios of the sensor with a positional shift;

FIGS. 14A to 14D are schematic views showing light irradiated parts when the azimuth is changed;

FIG. 15 is a plan view showing an arrangement of photodetectors and light irradiated parts with azimuths different from one another in a second preferred embodiment;

FIG. 16 is a graph showing a relationship between the azimuth and output ratios of a sensor in the second embodiment;

FIG. 17 is a plan view showing another arrangement



of photodetectors;

FIG. 18 is a plan view showing another arrangement of photodetectors;

FIG. 19 is a plan view showing an arrangement of  
5 photodetectors in a third preferred embodiment;

FIG. 20 is a plan view showing a sunlight sensor in a fourth preferred embodiment;

FIG. 21 is a graph showing relative sensitivities with respect to an elevation;

10 FIG. 22 is an explanatory view showing a sensor in a related art;

FIG. 23 is a graph showing a relationship between the azimuth and output ratios of the sensor with no positional shift in the related art;

15 FIGS. 24A to 24D are schematic views showing light irradiated parts when the azimuth is changed;

FIG. 25 is a graph showing a relationship between the azimuth and output ratios of the sensor with a positional shift;

20 FIGS. 26A to 26D are schematic views showing light irradiated parts when the azimuth is changed;

FIG. 27 is a schematic view for explaining the azimuth and the elevation;

FIG. 28 is a schematic view for explaining a  
25 relationship between the azimuth and a quantity of heat;  
and

FIG. 29 is a graph showing a sensor output with respect to the azimuth.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS  
(First Embodiment)

A sensor for detecting a quantity of light in a first preferred embodiment is useful for an automatic air conditioning system of a vehicle air conditioner. The automatic air conditioning system independently controls temperatures of air toward left side and right side passengers on front seats. When a passenger sets a temperature in a compartment at a specific value, blowout air temperatures and air amounts are automatically and independently controlled at the left side and the right side of the compartment by the air conditioning system. Accordingly, the side on which sunlight is incident has a lowered temperature to automatically correct the effect by the intensity of solar radiation, thereby keeping the temperature in the compartment constant.

FIGS. 1 and 2 show the sensor in the first embodiment. FIG. 1 is a plan view showing a state where an optical lens 4 and a slit plate (shading plate) 5 shown in FIG. 2 are detached. Referring to FIG. 2, the sensor 1 has a sensor housing 2 capable of functioning as a connector, a sensor chip 3, the optical lens 4, the slit plate 5, and terminals 6. The sensor housing 2 is composed of a case 7 and a holder 8, which are made of synthetic resin. The case 7 is a cylinder and stands when used. The holder 8 is inserted into an upper portion of the case 7. Since the sensor housing 2 is composed of the case 7 and the holder 8, it is possible to exchange only the holder 8 (a connector portion and a photodetector mounting portion) to match a

sensor specification using the case 7 as a common member.

Sensor attachment claws 9 are provided on the outer surface of the case 7. The sensor 1 is inserted into an attachment hole 10a of an instrument panel 10 of the vehicle in a direction X in FIG. 2, and is fixed therein by an urging force of the sensor attachment claws 9 applied outwardly.

The sensor chip 3 is disposed at the central portion of the upper surface of the holder 8. The terminals 6 are insert-molded with the holder 8 as output terminals to output sensor signals. The terminals are partially embedded in the holder 8. Each of the terminals 6 has an end exposed on the upper surface of the holder 8 and the other end protruding from the lower surface of the holder 8.

Referring to FIGS. 1 and 3, the rectangular sensor chip 3 has a right side photodetector  $D_R$  disposed at a left side of an axis  $L_{cent}$ , a left side photodetector  $D_L$  disposed at a right side of the axis  $L_{cent}$ , and a central photodetector  $D_c$  disposed on the axis  $L_{cent}$ . The axis  $L_{cen}$  is a reference of  $0^\circ$  azimuth. The photodetectors  $D_R$ ,  $D_L$ ,  $D_c$  respectively output signals corresponding quantities of light incident thereon. Photodiodes are used as the photodetectors  $D_R$ ,  $D_L$ ,  $D_c$ .

The sensor chip 3 is more specifically explained with reference to FIGS. 3 and 4. The sensor chip 3 is a photo IC including the photodetectors  $D_R$ ,  $D_L$ ,  $D_c$  and a signal processing circuit. The sensor chip 3 has an annular photo-detecting region 11, which is divided into photo-detecting regions 12, 13, 14 with an interior angle

of approximately  $120^\circ$ . The regions 12, 13, 14 are electrically insulated from one another. More specifically, as shown in FIG. 4, p type regions 12, 13, 14 are formed in a surface portion of an n type silicon substrate 15. A cathode electrode 16 is formed on the back surface of the silicon substrate 15, and anode electrodes 17, 18, 19 are respectively formed on the p type regions 12, 13, 14 at the main surface side of the silicon substrate 15. The photodetectors  $D_R$ ,  $D_L$ ,  $D_C$  are respectively formed in the p type regions 12, 13, 14, and output electric signals (photoelectric current) corresponding to the quantities of light incident on the regions 12, 13, 14. In FIG. 3, the signal processing circuit is formed at the outer circumference side of the annular photo-detecting region 11.

Referring again to FIG. 2, the slit plate 5 as a shading member is supported on the upper surface of the holder 8 to cover the sensor chip 3. The slit plate 5 is specifically shown in FIG. 5. The slit plate 5 is made of a shading material, and has a circular slit (through hole) 20 as a light transmittance portion penetrating through the central portion thereof. The slit 20 of the slit plate 50 is positioned just above the sensor chip 3 so that the center of the slit 20 is disposed on the axis  $L_{cent}$ .

The optical lens 4 is made of colored glass or resin (translucent material), and has a cup-like shape. The optical lens 4 fits the outer circumference surface of the case 7, and is supported by the housing 2 to be disposed

above the sensor chip 3. A recess 21 is formed at the central portion of the inner surface of the optical lens 4 to provide a lens function to the optical lens 4. The optical lens 4 may be composed of an aggregate lens (Fresnel lens) of prisms, or the like in stead of the concave lens to exhibit the lens function.

Light incident on the surface of the optical lens 4 in FIG. 2 passes through the optical lens 4 to be incident on the slit plate 5. Light passing through the slit 20 of the slit plate 5 then enters the photodetectors  $D_R$ ,  $D_L$ ,  $D_C$  (see FIG. 1). Accordingly, electric signals are outputted from the photodetectors  $D_R$ ,  $D_L$ ,  $D_C$ . That is, light incident on the sensor surface (optical lens 4) progresses within the lens 4 while changing its optical path according to the reflective index and the shape of the lens 4 and is radiated onto the sensor chip 3. The radiated light reaches the sensor chip 3 after passing through the slit 20 of the slit plate 5. Since the optical lens 4 is concave at a side where light is radiated therefrom, light entering from a horizontal direction (with a sensor elevation of  $0^\circ$ ) is also introduced to the sensor chip 3.

That is, as shown in FIG. 6, an optical path of light with an elevation of  $0^\circ$  is changed by the optical lens 4 so that the light is introduced to the sensor chip 3 through the slit 20 of the slit plate 5. As shown in FIG. 7, an optical path of light with an elevation of  $40^\circ$  is also changed by the optical lens 4 so that the light is introduced to the sensor chip 3. Similarly, light with an elevation of  $90^\circ$  is introduced to the sensor chip 3 as shown in FIG.

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FIG. 9 shows an electric constitution of the automatic air conditioning system in the present embodiment. The signal processing circuit 22 is connected to the three photodetectors  $D_R$ ,  $D_L$ ,  $D_C$ . In the signal processing circuit 22, an output current from the left side photodetector  $D_L$  and a half of an output current from the central photodetector  $D_C$  are added as a left side light signal output current ( $= I_L + 1/2 \cdot I_C$ ). The left side light signal output current is converted into a voltage by a resistor 25 whose value of resistance is  $R$ , and is transmitted to a microcomputer 23. An output current from the right side photodetector  $D_R$  and a half of the output current from the central photodetector  $D_C$  are added as a right side light signal output current ( $= I_R + 1/2 \cdot I_C$ ). The right side light signal output current is also converted into a voltage by the resistor 25 of  $R$  in the value of resistance, and is transmitted to the microcomputer 23.

That is, an output voltage is determined by the left side output voltage  $V1$  and the right side output voltage  $V2$ ,

which are represented by the following formulas:

$V1 = (\text{left side photodetector output current} + (\text{central photodetector output current})/2) \times R$ ; and

$V2 = (\text{right side photodetector output current} + (\text{central photodetector output current})/2) \times R$ .

Accordingly, the sum of the output voltages ( $=V1+V2$ ) is constant without depending on the direction from which light enters to the photo-detecting regions 12, 13,, 14.

Thus, the right side light signal is obtained by the output from the right side photodetector  $D_R$  and the output from the central photodetector  $D_C$  having small sensitivity. The left side light signal is obtained by the output from the left side photodetector  $D_L$  and the output from the central photodetector  $D_C$  having lowered sensitivity. The both signals cooperatively inform the intensity of solar radiation and the side where sunlight is incident on (driver's seat side or passenger's seat side). Specifically, the quantity of solar radiation is determined by the sum of the output signals ( $=V_1+V_2$ ), and the direction in which sunlight enters is determined by an output ratio ( $=V_1/(V_1+V_2)$  or  $V_2/(V_1+V_2)$ ).

The microcomputer 23 is connected to an air conditioning unit 24 including a blower, a cooler, a heater, and the like and mounted within the instrument panel of the vehicle. The microcomputer 23 inputs the two signals from the sensor 1, and controls the air conditioning unit 24 based on intensities of light incident on the left and right sides so that the side on which sunlight is incident (driver's seat side or passenger's seat side) receives an increased amount of air to have a lowered temperature.

FIG. 10 shows a constitution of the signal processing circuit 22 as an example. In the signal processing circuit 22, each of the photodetectors (diodes)  $D_R$ ,  $D_L$ ,  $D_C$  has a current mirror circuit, and a current mirror ratio of the current mirror circuit is adjusted to perform a gain adjustment. The sensitivity of the central photodetector  $D_C$  is lowered by controlling the gain of the signal outputted

from the central photodetector  $D_c$  to be smaller than those outputted from the other photodetectors  $D_R$ ,  $D_L$ .

Specifically, a current mirror circuit composed of transistors  $Q1$ ,  $Q2$  is connected to the photodetector  $D_L$ .

5 The transistor  $Q1$  is connected to the photodetector  $D_L$  in series. Likewise, a current mirror circuit composed of transistors  $Q3$ ,  $Q4$  is connected to the photodetector  $D_R$ , and a current mirror circuit composed of transistors  $Q5$ ,  $Q6$ ,  $Q7$  is connected to the photodetector  $D_c$ .

10 Emitter areas of the transistors  $Q2$ ,  $Q4$ ,  $Q6$ ,  $Q7$  are controlled to control the current mirror ratios. Specifically, when the transistors  $Q2$ ,  $Q4$ ,  $Q6$ ,  $Q7$  are formed in the sensor chip 3, the emitter areas of the transistors  $Q6$ ,  $Q7$  are controlled to be different from the  
15 emitter areas of the transistors  $Q2$ ,  $Q4$ . As a result, the gain of the current mirror circuit composed of the transistors  $Q1$ ,  $Q2$  is set at 1, the gain of the current mirror circuit composed of the transistors  $Q3$ ,  $Q4$  is set at 1, and the gain of the current mirror circuit composed  
20 of the transistors  $Q5$ ,  $Q6$ ,  $Q7$  is set at 0.5. The sum of currents flowing in the transistors  $Q2$ ,  $Q6$  is amplified by a current mirror circuit composed of transistors  $Q8$ ,  $Q9$ , and then is outputted. The sum of currents flowing in the transistors  $Q4$ ,  $Q7$  is amplified by a current mirror  
25 circuit composed of transistors  $Q10$ ,  $Q11$ , and then is outputted.

Next, operation of the sensor 1 described above will be explained. As shown in FIGS. 6 to 8, light incident on the lens 4 is introduced to the photodetectors  $D_R$ ,  $D_L$ ,



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D<sub>c</sub> through the slit 20 of the slit plate 5. Each of the photodetectors D<sub>R</sub>, D<sub>L</sub>, D<sub>c</sub> receives light and respectively convert it into signals corresponding to the quantity of light incident thereon. Further, in the signal processing circuit 22 shown in FIG. 9, the left side light signal V1 is obtained by the output from the left side photodetector D<sub>L</sub> and the output from the central photodetector D<sub>c</sub> having small sensitivity. The right side light signal V2 is obtained by the output from the right side photodetector D<sub>R</sub> and the output from the central photodetector D<sub>c</sub>. The microcomputer 23 detects the quantity and the direction of solar radiation to perform the left side and right side independent controls of the air conditioner, i.e., to independently air-condition the right and left seats based on the detected quantity of light.

Next, characteristics of the sensor 1 when the slit 20 of the slit plate 5 is offset from the axis L<sub>cent</sub> to cause a positional shift between the slit plate 5 and the photodetectors D<sub>R</sub>, D<sub>L</sub>, D<sub>c</sub> will be explained. FIG. 11 shows a relationship between azimuth  $\phi$  and right side and left side output ratios CR1<sub>R</sub>, CR1<sub>L</sub> when there is no positional shift between the slit plate 5 and the photodetectors D<sub>R</sub>, D<sub>L</sub>, D<sub>c</sub>. The light irradiated parts in cases where azimuth  $\phi$  is 0°, 30°, 60°, 90° are shown in FIGS. 12A to 12D, and the output ratios CR1<sub>R</sub>, CR1<sub>L</sub> are shown in FIG. 11. The right side and left side output ratios CR1<sub>R</sub>, CR1<sub>L</sub> in the present embodiment are represented by the following formulas:

$$CR1_R = ((C_R + 0.5 \cdot C_c) \times R) / ((C_R + C_L + C_c) \times R) = V2 / (V1 + V2)$$

$$CR1_L = ((C_L + 0.5 \cdot C_c) \times R) / ((C_R + C_L + C_c) \times R) = V1 / (V1 + V2)$$

Here,  $C_R$  is an output current from the right side photodetector  $D_R$ ,  $C_L$  is an output current from the left side photodetector  $D_L$ , and  $C_C$  is an output current from the central photodetector  $D_C$ . When azimuth  $\phi$  is  $0^\circ$ , the output ratios  $CR_{1R}$ ,  $CR_{1L}$  are 0.50, respectively.

On the other hand, FIG. 13 shows a relationship between azimuth  $\phi$  and right side and left side output ratios  $CR_{1R}$ ,  $CR_{1L}$  when there arises a positional shift between the slit plate 5 and the photodetectors  $D_R$ ,  $D_L$ ,  $D_C$ . The light irradiated parts in cases where azimuth  $\phi$  is  $0^\circ$ ,  $30^\circ$ ,  $60^\circ$ ,  $90^\circ$  with a positional shift of 0.1 mm are shown in FIGS. 14A to 14D, and the output ratios  $CR_{1R}$ ,  $CR_{1L}$  in those cases are shown in FIG. 13. When azimuth  $\phi$  is  $0^\circ$ , the right side and left side output ratios  $CR_{1R}$ ,  $CR_{1L}$  are 0.53 and 0.47, respectively. The right side and left side output ratios  $CR_R$ ,  $CR_L$  of the sensor shown in FIG. 22 with the same shift ( $=0.1$  mm) were, as shown in FIG. 25, 0.60 and 0.40, respectively when azimuth  $\phi$  was  $0^\circ$ . Accordingly, it is confirmed that the difference between the right side and left side output ratios  $CR_{1R}$ ,  $CR_{1L}$  is decreased when azimuth  $\phi$  is  $0^\circ$  and when there is a positional shift between the slit plate 5 and the photodetectors  $D_R$ ,  $D_L$ ,  $D_C$ .

Comparing FIGS. 11 and 23, the characteristics shown in FIG. 11 change with respect to a change in azimuth more linearly than those in FIG. 23. The reason is considered as follows. In the case shown in FIG. 23, the right side light signal is obtained only by the output from the right side photodetector  $D_R$ , and the left side light signal is obtained only by the output from the left side

photodetector  $D_L$ . On the other hand, in the present embodiment shown in FIG. 11, sensitivities of the right side and left side light signals are depressed at a portion adjacent to the axis  $L_{cent}$  (around  $0^\circ$  azimuth) by the output from the central photodetector  $D_c$ , sensitivity of which is lowered. Correctly, the sensitivities of the right side and left side light signals are depressed most when the azimuth is  $0^\circ$ , and the degree of depression decreases as the azimuth is increased.

Thus, the central photodetector (common detecting element)  $D_c$  makes it difficult to produce the difference between the right side and left side light signals at the central detecting part (having an azimuth in a range of approximately  $0^\circ$  to  $\pm 30^\circ$ ). As a result, the effect by the assembling shift (offset from the center) is moderated. The sensor characteristics are not liable to be affected by the positional shift between the slit plate 5 and the photodetectors  $D_R$ ,  $D_L$ ,  $D_c$ , resulting in high accuracy for independently air-conditioning the left side and right side in the compartment.

The detection characteristics can be approached to the ideal state shown in FIG. 29 by providing the central photodetector (common detecting element)  $D_c$ . That is, when the azimuth is small, light is incident on the portion adjacent to the reference axis  $L_{cent}$ . In this case, as shown in FIG. 11, the difference between the left side and right side light signals is small. When the azimuth becomes large to some extent, the difference between the light signals becomes also large. This makes it possible to

approach the detection characteristics to the ideal state as compared to the case shown in FIG. 23.

(Second Embodiment)

A second preferred embodiment will be explained focusing on differences from the first embodiment.

As shown in FIG. 15, an area of each light irradiated part A1 to A5 is reduced with respect to the photodetectors by reducing the diameter of the slit 20 of the slit plate 5. Accordingly, in a relationship between azimuth and output ratios shown in FIG. 16, changes in output ratios are decreased when the azimuth is in a range of  $0^\circ$  to  $30^\circ$ , thereby approaching the ideal state more than that shown in FIG. 11. The intensity of light incident on the light irradiated part indicated with A4 when the azimuth is  $60^\circ$  is assumed to be maximum for the photodetectors  $D_R$ ,  $D_L$ , and the area of the light irradiated part is not increased to A5 when the azimuth is  $90^\circ$ . The photodetectors  $D_R$ ,  $D_L$ ,  $D_C$  are arranged into an annular shape; however, they may be arranged into other shapes such as a rectangle as shown in FIG. 17, or may be arranged entirely on the sensor chip 3 as shown in FIG. 18.

(Third Embodiment)

A third preferred embodiment will be explained focusing on differences from the first and second embodiments.

As shown in FIG. 19, the right side and left side photodetectors  $D_R$ ,  $D_L$  are respectively disposed on the left and right sides of the axis  $L_{cent}$ , which is a reference when the azimuth is  $0^\circ$ . The left side and right side

photodetectors  $D_R$ ,  $D_L$  are alternately disposed at a specific portion, a half width of which is  $L/2$  from the axis  $L_{cent}$ . Specifically, the right side photodetector  $D_R$  has a rectangular part 30 with a width  $W$ , and the right side surface of the rectangular part 30 is formed into a saw-tooth shape having several isosceles triangle teeth 31. Likewise, the left side photodetector  $D_L$  has a rectangular part 32 with a width  $W$ , and the left side surface of the rectangular 32 is formed into a saw-tooth shape having several isosceles triangle teeth 33. The saw-tooth part of the right side photodetector  $D_R$  and the saw-tooth part of the left side photodetector  $D_L$  are disposed on the axis  $L_{CENT}$  to fit each other.

The sensor described above is operated to detect a quantity of light as follows.

As shown in FIG. 7, light enters the photodetectors  $D_L$ ,  $D_R$  shown in FIG. 19 after passing through the slit 20 of the slit plate 5. The left side and right side photodetectors  $D_L$ ,  $D_R$  then convert light incident thereon into signals corresponding to quantities of the light. The right side light signal is obtained by the output from the right side photodetector  $D_R$ , and the left side light signal is obtained by the output from the left side photodetector  $D_L$ . In the microcomputer 23 shown in FIG. 9, the quantity of solar radiation is determined by the sum of the right side and left side light signals, and the direction (right side or left side) of sunlight is determined by the output ratio between both signals. Then, the microcomputer 23 controls the air conditioning unit

24 (see FIG. 9) to independently air-conditioning right and left seats in the compartment.

At that time, there may arise a positional shift between the slit plate 5 and the photodetectors  $D_L$ ,  $D_R$ .

5 That is, the center of the slit 20 of the slit plate 5 may be offset from the axis  $L_{CENT}$ . Even in such a case, the right side and left side light signals in the present embodiment are less susceptible to the positional shift as compared to the case where the left side and right side photodetectors  $D_L$ ,  $D_R$  are divided by the axis  $L_{CENT}$  as shown in FIG. 22. This is because the saw-tooth parts of the left side and right side photodetectors  $D_L$ ,  $D_R$  are alternately disposed along the axis  $L_{CENT}$  with a specific width  $L$  to blunt the sensitivity along the axis  $L_{CENT}$ . When 15 the positional shift is not considered, light is incident on the vicinity of the axis  $L_{CENT}$  with a small azimuth. In this case, the difference between both light signals is small. As the azimuth is increased, the difference between both light signals is also increased, thereby 20 approaching the ideal detection characteristics shown in FIG. 29.

#### (Fourth Embodiment)

Next, a fourth preferred embodiment will be explained focusing on differences from the first and second 25 embodiments. FIG. 20 shows a sensor (sensor chip) 3a in the present embodiment. The sensor 3a is mounted on a vehicle as a sunlight sensor for independently air-conditioning right and left seats of the vehicle. The sensor 3a is further used as an automatic lighting sensor

for automatically turning on or off a headlamp of the vehicle. The sensor 3a in the present embodiment has the two functions described above. FIG. 21 shows relative sensitivities of this sensor with respect to an elevation, i.e., elevation characteristics.

Detailed explanation is below. Referring to FIG. 20, the sensor chip 3a has a circular center photo-detecting region (photodetector) 40, and arc-like photo-detecting regions (photodetectors) 41, 42, 43 provided around the region 40, and arc-like photo-detecting regions (photodetectors) 44, 45, 46 provided around the regions 41, 42, 43. The regions 40, 42, 45 are disposed on an axis  $L_{CENT}$  as a reference when the azimuth is  $0^\circ$ . The axis  $L_{CENT}$  extends in a front-rear direction of the vehicle. The arc-like photo-detecting regions 41, 42, 43 are separated from the circular photo-detecting region 40 at a specific distance  $d_1$ . The regions 43, 46 compose a right side photodetector  $D_R$ , and the regions 41, 44 compose a left side photodetector  $D_L$ . The regions 42, 45 compose a first central photodetector  $D_{c1}$  and the region 40 composes a second central photodetector  $D_{c2}$ .

As to detection of direction, the effect by a positional shift (assembling shift) between a shading member and the photodetectors is lessened by providing the inside arc-like photo-detecting regions 41 - 43 with respect to the outside arc-like photo-detecting regions 44 - 46. The effect by the assembling shift is further lessened by providing the circular photodetector 40 at the inside of the arc-like photo-detecting regions 41 - 43.

Increasing the area of the circular photo-detecting region 40 effectuates to increase a permitted range of the assembling shift.

As described above, in the present embodiment, since several (three) central photodetectors  $D_c$  are provided on the axis  $L_{CENT}$ , left side and right side light signals are less susceptible to the positional shift between the slit plate 5 and the photodetectors  $D_L$ ,  $D_R$  accompanying the offset of the slit 20 of the slit plate 5 from the axis  $L_{CENT}$  as compared to the case where the left side and right side photodetectors  $D_L$ ,  $D_R$  are divided by the axis  $L_{CENT}$  as shown in FIG. 22.

As to the elevation characteristics, the circular photo-detecting region 40 is used for directional characteristics (I) in FIG. 21, and the photo-detecting regions 40 - 46 are used for directional characteristics (II) in FIG. 21. The circular photo-detecting region 40 is common for obtaining the both characteristics (I), (II). The directional characteristics (I) has low output (sensitivity) at a small elevation, and high sensitivity at a large elevation. This directional characteristics (I) is used for automatic lighting. The directional characteristics (II) has a peak at a specific elevation (around  $35^\circ$  in FIG. 21), and is used for the sunlight sensor. The microcomputer 23 turns on or off the headlamp and the like of the vehicle using the directional characteristics (I), and air-conditions the right and left seats independently using the directional characteristics (II). Accordingly, one sensor can control several control



targets (air conditioning unit and headlamp) with the multipurpose center element 40. The photodetectors 40-46 in the present embodiment are preferably composed of diodes.

5 On the other hand, referring again to FIG. 20, a region 47 provided at the vehicle front side along the axis  $L_{CENT}$  has no photo-detecting region thereon, and a signal processing circuit is formed at the region 47 for processing the signals outputted from the photodetectors.

10 Photoelectric currents produced by solar radiation on the photo-detecting regions are processed in the signal processing circuit. The reason why no photo-detecting region is provided at the region 47 is because sunlight enters the region 47 not from the vehicle front side but

15 from the vehicle rear side by the function of the slit 20 of the silt plate 5 and the optical lens 4.

Thus, although the region 47 is a dead space for the photo-detecting region, and does not contribute to the output characteristics of the sensor, the region 47 is

20 effectively used to have the signal processing circuit therein. Accordingly, a region for holding the signal processing circuit, which has been provided at an outside of an annular photo-detecting region, can be omitted, resulting in size reduction. This is especially effective

25 to a sensor including photodetectors and a signal processing circuit integrated therein.

In the present embodiment, although the first central photodetectors  $D_{c1}$  (regions 42, 45) and the second central photodetector  $D_{r2}$  (region 40) are separately provided to

exhibit the two directional characteristics shown in FIG. 21, the region 40 may be connected to the regions 42, 45 provided that the elevation characteristics are not required. In the embodiments described above, each  
5 element is composed of a photo-diode; however, it may be composed of another element such as a phototransistor.

While the present invention has been shown and described with reference to the foregoing preferred  
10 embodiments, it will be apparent to those skilled in the art that changes in form and detail may be made therein without departing from the scope of the invention as defined in the appended claims.